IPM Model – Updates to Cost and Performance for APC Technologies

SCR Cost Development Methodology for Oil/Gas-fired Boilers

Final

February 2023

Project 13527-002

Eastern Research Group, Inc.

Prepared by

55 East Monroe Street • Chicago, IL 60603 USA • 312-269-2000

LEGAL NOTICE

This analysis ("Deliverable") was prepared by Sargent & Lundy, L.L.C. ("S&L"), expressly for the sole use of Eastern Research Group, Inc. ("Client") in accordance with the agreement between S&L and Client. This Deliverable was prepared using the degree of skill and care ordinarily exercised by engineers practicing under similar circumstances. Client acknowledges: (1) S&L prepared this Deliverable subject to the particular scope limitations, budgetary and time constraints, and business objectives of the Client; (2) information and data provided by others may not have been independently verified by S&L; and (3) the information and data contained in this Deliverable are time sensitive and changes in the data, applicable codes, standards, and acceptable engineering practices may invalidate the findings of this Deliverable. Any use or reliance upon this Deliverable by third parties shall be at their sole risk.

This work was funded by U.S. Environmental Protection Agency (EPA) through Eastern Research Group, Inc. (ERG) as a contractor and reviewed by ERG and EPA personnel.

Sargent & Lundy

Oil/Gas-fired SCR Cost Development Methodology

Purpose of IPM Model

Cost algorithms in the IPM model are based primarily on a statistical evaluation of cost data available from various industry publications, and do not take into consideration site-specific cost issues. The primary purpose of the IPM cost modules is to provide generic order-of-magnitude costs for various air quality control technologies that can be applied to the electric power generating industry on a system-wide basis, not on an individual unit basis. By necessity, the cost algorithms were designed to require minimal site-specific information. The IPM cost equations can provide order-of-magnitude capital costs for various air quality control systems based only on a limited number of inputs such as unit size, gross heat rate, inlet NOx level, fuel sulfur level, % removal efficiency, fuel type, and a subjective retrofit factor. The outputs from these equations represent the “average” costs associated with the “average” project scope for the subset of data utilized in preparing the equations. The IPM cost equations do not account for site-specific factors that can significantly impact costs, such as flue gas volume, temperature and do not address regional labor productivity, local workforce characteristics, local unemployment and labor availability, project complexity, local climate, and working conditions. Finally, the indirect capital costs included in the IPM cost equations do not account for all project-related indirect costs a facility would incur to install a retrofit control such as project contingency.

Establishment of Cost Basis

The arrangement of SCR technology at oil/gas-fired boilers can potentially be applied as an in-line configuration if space allows; however, in the vast majority of retrofit situations this is not feasible and could only be established by performing a more detailed engineering evaluation of a specific facility. Therefore, the application of SCR technology to oil/gas-fired boilers is similar to coal-fired applications in that a separate reactor is required. However, there are expected to be significant differences in costs categories due to a few factors. Oil and gas-fired units have relatively low particulate matter and, in most cases, sulfur, therefore, the catalyst requirements are different than coal-fired applications. Smaller pitch catalyst can be used resulting in a lower volume of catalyst being required. In most cases, a single layer of catalyst can be used, resulting in much smaller reactors than coal-fired applications with fewer flue gas mixing devices. Furthermore, this reduces the size of new fans for the additional pressure drop. Finally, because the flue gas in very low in sulfur compounds, all air heater and acid-gas mitigation referenced in the coal-fired SCR system is not applicable. As such, the 2021 coal-fired boilers IPM SCR module was used as input to this module along with S&L in-house information for oil and gas applications to adjust the cost factors.

Finally, this module was benchmarked against recent SCR projects to confirm the applicability to the current market conditions. The S&L in-house database of oil/gas boilers SCR project costs were converted to 2021 dollars based on an escalation factor of 2.5% based on the industry trends over the last ten years (2010 – 2020) excluding the current market conditions.[1]

The costs for retrofitting a plant smaller than 100 MW increase rapidly due to the economy of size. Oil and gas boilers generally have more compact sites with very short flue gas ducts running from the boiler house to the chimney. Because of the limited space, the SCR reactor and new duct work can be expensive to design and install. Additionally, the plants might not have enough margins in the fans to overcome the pressure drop due to the duct work configuration and SCR reactor and therefore new fans may be required.

[1] To escalate prices from Jan 2021 to July 2022 costs, an escalation factor of 19.5% should be used, based on the Handy Whitman steam production plant index.

Oil/Gas-fired SCR Cost Development Methodology

The least squares curve fit was based upon an average of the SCR retrofit projects in recent years. Retrofit difficulties associated with an SCR may result in significant capital cost increases. A typical SCR retrofit was based on:

- Retrofit Difficulty = 1 (Average retrofit difficulty);
- Gross Heat Rate = 9500 Btu/kWh;
- Type of Fuel = Natural Gas and Oil; and
- Project Execution = Multiple lump sum contracts.

Methodology

Inputs

To predict SCR retrofit costs several input variables are required. The unit size in MW is the major variable for the capital cost estimation followed by the type of fuel (Natural Gas or Oil) which will influence the flue gas quantities as a result of the different typical heating values. The unit heat rate factors into the amount of flue gas generated and ultimately the size of the SCR reactor and reagent preparation. A retrofit factor that equates to difficulty in construction of the system must be defined. The NOx rate and removal efficiency will impact the amount of catalyst required and size of the reagent handling equipment.

The cost methodology is based on a unit located within 500 feet of sea level. The actual elevation of the site should be considered separately and factored into the cost due to the effects on the flue gas volume. The base SCR and balance of plant costs are directly impacted by the site elevation. These two base cost modules should be increased based on the ratio of the atmospheric pressure between sea level and the unit location. As an example, a unit located 1 mile above sea level would have an approximate atmospheric pressure of 12.2 psia. Therefore, the base SCR and balance of plant costs should be increased by:

14.7 psia/12.2 psia = 1.2 multiplier to the base SCR and balance of plant costs

The NOx removal efficiency specifically affects the SCR catalyst, reagent and steam costs. The lower level of NOx removal is expected to range from 0.02 lb NOx/MMBtu to 0.05 lb NOx/MMBtu; however, this depends on the inlet NOx concentration. The highest efficiency that could be achieved with oil/gas-fired boilers is approximately 90-95%.

Outputs

Total Project Costs (TPC)

First the installed costs are calculated for each required base module. The base module installed costs include:

- All equipment;
- Installation;
- Buildings;
- Foundations;
- Electrical; and
- Average retrofit difficulty.

Oil/Gas-fired SCR Cost Development Methodology

The base modules are:

BMR =	Base SCR cost
BMF =	Base reagent preparation cost
BMB =	Base balance of plant costs including: ID or booster fans, ductwork reinforcement, piping, etc…
BM =	BMR + BMF + BMA + BMB

The total base module installed cost (BM) is then increased by:

- Engineering and construction management costs at 10% of the BM cost;
- Labor adjustment for 6 x 10-hour shift premium, per diem, etc., at 10% of the BM cost; and
- Contractor profit and fees at 10% of the BM cost.

A capital, engineering, and construction cost subtotal (CECC) is established as the sum of the BM and the additional engineering and construction fees[2].

Additional costs and financing expenditures for the project are computed based on the CECC. Financing and additional project costs include:

- Owner's home office costs (owner's engineering, management, and procurement) at 5% of the CECC; and
- Allowance for Funds Used During Construction (AFUDC) at 6% of the CECC and owner's costs. The AFUDC is based on a two-year engineering and construction cycle.

The total project cost is based on a multiple lump sum contract approach. Should a turnkey engineering procurement construction (EPC) contract be executed, the total project cost could be 10 to 15% higher than what is currently estimated.

Escalation is not included in the estimate. The total project cost (TPC) is the sum of the CECC and the additional costs and financing expenditures.

Fixed O&M (FOM)

The fixed operating and maintenance (O&M) cost is a function of the additional operations staff (FOMO), maintenance labor and materials (FOMM), and administrative labor (FOMA) associated with the SCR installation. The FOM is the sum of the FOMO, FOMM, and FOMA.

The following factors and assumptions underlie calculations of the FOM:

- All of the FOM costs were tabulated on a per kilowatt-year (kW yr) basis.
- In general, half of an operator's time is required to monitor a retrofit SCR. The FOMO is based on that ½ time requirement for the operations staff.
- The fixed maintenance materials and labor is a direct function of the process capital cost at 0.5% of the BM for units less than 300 MW and 0.3% of the BM for units greater than or equal to 300 MW and.

[2] Generally, the direct cost of labor versus material/equipment is 50% material/equipment and 50% labor. Note that this is only direct cost and does not include all the project/construction indirect costs. The 50% material/equipment typically breaks down into major categories as follows: Demolition/civil work/concrete: ~5%, Steel: ~20%, Electrical/Wires/Instrumentation: ~ 9%, Mechanical equipment: ~14%, Piping/Insulation: ~2%

Oil/Gas-fired SCR Cost Development Methodology

- The administrative labor is a function of the FOMO and FOMM at 3% of (FOMO + 0.4FOMM).

Variable O&M (VOM)

Variable O&M is a function of:

- Reagent use and unit costs;
- Catalyst replacement and disposal costs;
- Additional power required and unit power cost; and
- Steam required and unit steam cost.

The following factors and assumptions underlie calculations of the VOM:

- All of the VOM costs were tabulated on a per megawatt-hour (MWh) basis.
- The reagent consumption rate is a function of unit size, NOx feed rate and removal efficiency.
- The catalyst replacement and disposal costs are based on the NOx removal and total volume of catalyst required.
- The additional power required includes increased fan power to account for the added pressure drop and the power required for the reagent supply system. These requirements are a function of gross unit size and actual gas flow rate.
- The additional power is reported as a percent of the total unit gross production. In addition, a cost associated with the additional power requirements can be included in the total variable costs.
- The steam usage is based upon reagent consumption rate.

Input options are provided for the user to adjust the variable O&M costs per unit. Average default values are included in the base estimate. The variable O&M costs per unit options are:

- Urea cost in $/ton;
- Catalyst costs that include removal and disposal of existing catalyst and installation of new catalyst in $/cubic meter;
- Auxiliary power cost in $/kWh;
- Steam cost in $/1000 lb; and
- Operating labor rate (including all benefits) in $/hr.

The variables that contribute to the overall VOM are:

VOMR =	Variable O&M costs for urea reagent
VOMW =	Variable O&M costs for catalyst replacement & disposal
VOMP =	Variable O&M costs for additional auxiliary power
VOMM =	Variable O&M costs for steam

The total VOM is the sum of VOMR, VOMW, VOMP, and VOMM. Table 1 is a complete capital and O&M cost estimate worksheet.

Sargent & Lundy

Oil/Gas-fired SCR Cost Development Methodology

Table 1. Example Complete Cost Estimate for an SCR System

Variable	Designation	Units	Value	Calculation
Unit Size	A	(MW)	500	<--- User Input
Retrofit Factor	B		1	<--- User Input (An "average" retrofit has a factor = 1.0)
Heat Rate	C	(Btu/kWh)	9500	<--- User Input
NOx Rate	D	(lb/MMBtu)	0.3	<--- User Input
SO2 Rate	E	(lb/MMBtu)	3	<--- User Input
Type of Fuel	F		Natural gas	<--- User Input
Fuel Factor	G		1.00	Natural Gas=1.0, Oil=1.06
Heat Rate Factor	H		0.95	C/10000
Heat Input	I	(Btu/hr)	4.75E+09	A*C*1000
NOx Removal Efficiency	K	(%)	90	<--- User Input, Note to user: maximum removal efficiency is 90-95%
NOx Removal Factor	L		1.125	K/80
NOx Removed	M	(lb/hr)	1283	D*I/10^6*K/100
Urea Rate (100%)	N	(lb/hr)	896	M*0.525*60/46*1.01/0.99
Steam Required	O	(lb/hr)	1014	N*1.13
Aux Power **Include in VOM?** ☑	P	**(%)**	**0.27**	0.28*(G*H)^0.43
Urea Cost (50% wt solution)	R	($/ton)	350	<--- User Input
Catalyst Cost	S	($/m3)	9000	<--- User Input (Includes removal and disposal of existing catalyst and installation of new catalyst)
Aux Power Cost	T	($/kWh)	0.06	<--- User Input
Steam Cost	U	($/klb)	4	<--- User Input
Operating Labor Rate	V	($/hr)	60	<--- User Input (Labor cost including all benefits)

Costs are all based on 2021 dollars

Capital Cost Calculation		**Example**		**Comments**
Includes - Equipment, installation, buildings, foundations, electrical, and retrofit difficulty.				
BMR ($) =	129500*(B)*(L)^0.2*(A*G*H)^0.92	$	38,464,000	SCR (ductwork modifications and strengthening, reactor, bypass) island cost
BMF ($) =	671000*(M)^0.25	$	4,015,000	Base reagent preparation cost
BMB ($) =	315000*(B)*(A*G*H)^0.42	$	4,193,000	ID or booster fans & auxiliary power modification costs
BM ($) =	BMR + BMF + BMA + BMB	$	46,672,000	Total bare module cost including retrofit factor
BM ($/KW) =			93	Base cost per kW
Total Project Cost				
A1 = 10% of BM		$	4,667,000	Engineering and Construction Management costs
A2 = 10% of BM		$	4,667,000	Labor adjustment for 6 x 10 hour shift premium, per diem, etc…
A3 = 10% of BM		$	4,667,000	Contractor profit and fees
CECC ($) = BM+A1+A2+A3		**$**	**60,673,000**	Capital, engineering and construction cost subtotal
CECC ($/kW) =			**121**	Capital, engineering and construction cost subtotal per kW
B1 = 5% of CECC		$	3,034,000	Owners costs including all "home office" costs (owners engineering, management, and procurement activities)
TPC' ($) - Includes Owner's Costs = CECC + B1		$	63,707,000	Total project cost without AFUDC
TPC' ($/kW) - Includes Owner's Costs =			**127**	Total project cost per kW without AFUDC
B2 = 6% of (CECC + B1)		$	3,822,000	AFUDC (Based on a 2 year engineering and construction cycle)
C1 = 15% of CECC + B1		$	-	EPC fees of 15%
TPC ($) = CECC + B1 + B2		**$**	**67,529,000**	Total project cost
TPC ($/kW) =			**135**	Total project cost per kW

Oil/Gas-fired SCR Cost Development Methodology

Variable	Designation	Units	Value	Calculation
Unit Size	A	(MW)	500	<--- User Input
Retrofit Factor	B		1	<--- User Input (An "average" retrofit has a factor = 1.0)
Heat Rate	C	(Btu/kWh)	9500	<--- User Input
NOx Rate	D	(lb/MMBtu)	0.3	<--- User Input
SO2 Rate	E	(lb/MMBtu)	3	<--- User Input
Type of Fuel	F		Natural gas	<--- User Input
Fuel Factor	G		1.00	Natural Gas=1.0, Oil=1.06
Heat Rate Factor	H		0.95	C/10000
Heat Input	I	(Btu/hr)	4.75E+09	A*C*1000
NOx Removal Efficiency	K	(%)	90	<--- User Input, Note to user: maximum removal efficiency is 90-95%
NOx Removal Factor	L		1.125	K/80
NOx Removed	M	(lb/hr)	1283	D*I/10^6*K/100
Urea Rate (100%)	N	(lb/hr)	896	M*0.525*60/46*1.01/0.99
Steam Required	O	(lb/hr)	1014	N*1.13
Aux Power **Include in VOM?** ☑	P	**(%)**	**0.27**	0.28*(G*H)^0.43
Urea Cost (50% wt solution)	R	($/ton)	350	<--- User Input
Catalyst Cost	S	($/m3)	9000	<--- User Input (Includes removal and disposal of existing catalyst and installation of new catalyst)
Aux Power Cost	T	($/kWh)	0.06	<--- User Input
Steam Cost	U	($/klb)	4	<--- User Input
Operating Labor Rate	V	($/hr)	60	<--- User Input (Labor cost including all benefits)

Costs are all based on 2021 dollars

Fixed O&M Cost

FOMO ($/kW yr) = (1/2 operator time assumed)*2080*V/(A*1000)	$	0.13	Fixed O&M additional operating labor costs
FOMM ($/kW yr) = (IF A < 300 then 0.005*BM ELSE 0.003*BM)/(B*A*1000)	$	0.28	Fixed O&M additional maintenance material and labor costs
FOMA ($/kW yr) = 0.03*(FOMO+0.4*FOMM)	$	0.01	Fixed O&M additional administrative labor costs
FOM ($/kW yr) = FOMO + FOMM + FOMA	**$**	**0.41**	Total Fixed O&M costs

Variable O&M Cost

VOMR ($/MWh) = N*R/(A*1000)	$	0.63	Variable O&M costs for Urea
VOMW ($/MWh) = (0.065*(G^2.9)*(L^0.71)*S)/(8760)	$	0.07	Variable O&M costs for catalyst: replacement & disposal
VOMP ($/MWh) =P*T*10	$	0.16	Variable O&M costs for additional auxiliary power required including additional fan power
VOMM ($/MWh) = O*U/A/1000	$	0.01	Variable O&M costs for steam
VOM ($/MWh) = VOMR + VOMW + VOMP + VOMM	**$**	**0.87**	