A STUDY ON FSW PARAMETERS OF JOINING DISSIMILAR METALS - AL AND FE

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ABSTRACT

The materials with similar and dissimilar qualities are joined effectively in their solid-state by Friction Stir Welding (FSW). FSW eliminates the conventional problems and produces crack-free and completely solidified joints. In recent years the commercialization of FSW is focused on metals like Fe and Al-based alloys. However, to commercialize such a process numerous research studies are required to characterize and establish process windows. FSW process is suitable for joining the different materials having different mechanical and chemical properties and for different material structures. In general, aerospace applications require hybrid metal joints to offer high strength – high ductile properties by joining varied metal alloys. FSW is the feasible way to join such metals to get high properties. This review mainly provides the feasibility of the FSW technique to join the different materials/alloys.

Key Words: FSW, Aluminium, Steel, Process parameters, tensile strength.

1. Introduction

Friction Stir welding and its types were invented by The Welding Institute (TWI), in 1991 with an objective to join varied metal combinations like Al, Steel, Cu, Mg, and Ti in the solid-state [1]. In FSW, the materials to be joint are softened by the frictional heat generated by the stirring action of the simple tool with combined tool rotational and tool traverse movements. The presence of solidification, porosity defects, and intermetallic compounds in the fusion welding of Al has been overcome by FSW with an additional ability to join with hard metals like Fe. The merits of FSW include less energy requirement, less pollution, low cost, and easy procedure.

Unlike Shielded Metal Arc Welding (SMAW), the need for skilled operators and costly equipment are replaced with common fixtures, tool rotating spindle, and semi-skilled person to perform metal joining in FSW.

However, combination of alloys have important applications in the aerospace, automobile, and shipbuilding industries. In all these applications it becomes necessary to get the higher performance of the welded joints. The main advantage of using

dissimilar materials in welding structures is to reap the advantages of the combined properties of both materials.

The factors which mainly influence the welding quality in FSW (Fig.1) are as follows:

- Material behavior on joining.
- Ability to form intermetallic compounds.
- Thermal conductivity
- Material positioning in advance and retreating side.
- Tool terminology: Shoulder pin, angle
- Welding parameters: rpm, traverse speed.

Fig. 1 Schematic diagram of FSW Setup

2. Principle of operation

Friction stir welding (FSW) is a solid-state joining process that uses a non-consumable rotating and traversing tool to the faces of the workpieces without melting them. The profiled pin called probe at the front end of the rotating tool performs the metal joining. The diameter and length of the probe are kept smaller than the respective dimensions of the shoulder. The probe of the rotating tool is fed into the joining faces of the clamped workpieces until the shoulder touches the surface of the workpieces. Although the probe is shorter it should be less than the weld plate thickness to prevent tearing of the joint during tool movement. After the start of the welding, a short dwell time is given to enable the metal to soften, and then the tool is moved forward at a constant speed along the joint line [2].

As mentioned earlier, the frictional heat generated between the tool and the workpiece softens the joint region near the FSW tool. The softening of the metal leads to plasticizing the region in the direction of leading to the rear with high force helps in forged consolidation of the weld. The process of metal softening, plasticizing, and consolidation is continuous along the path of tool traverse resulting in dynamic recrystallization of solid-state deformation of the metal.

On the tool traverse along the joint line, the probe mixes the plasticized material mechanically,

and compresses the hot and softened metal by the mechanical pressure to form a solid-state joint. This type of joint is highly preferred to join dissimilar materials aiming at structures with high strength. Thus, FSW is predominately used in the joining of Al, Cu, Ti alloys, mild steel, stainless steel, and magnesium alloys [3]. More recently, it was successfully used in the joining of polymers. In addition, the joining of dissimilar metals, such as aluminium to magnesium alloys, has been recently achieved by FSW.

3. FSW Process parameters

The commonly considered process parameters in FSW are listed below and discussed in the following section. Fig. 2 illustrates the schematic of the terms involved in FSW

1. Tool design and geometry
2. Welding / transverse speed
3. Plunge depth
4. Axial tool's Plunge force
5. Tool tilt angle
6. Dwell time.

Fig. 2 FSW tool terminology

3.1 Tool design and geometry

The design of the tool is a critical factor, as a good tool can improve both the quality of the weld and the maximal possible welding speed. Fig. 3, depicts the criterion necessarily considered in the selection of the FSW tool. The FSW tool should have high strength, toughness, hot wear resistance, good oxidation resistance, and low thermal conductivity to minimize heat loss and thermal damage to the machinery [4].

Fig. 3. FSW tool criterion

The design of the tool is a critical factor, a good tool can improve both the quality of the weld and maximize the possible welding speed. Fig. 4 illustrates the possible tool geometry tried in FSW process [5].

Hot-worked tool steel such as AISI H13 has proven to be good for welding Al alloys in the

thickness range from 0.5 to 50 mm, whereas advanced tool materials are necessary for highly demanding applications such as highly abrasive metal matrix composites or higher-melting-point materials such as steel or titanium.

Fig. 4 FSW tool geometry

3.2 Welding speed or Traverse speed

Welding speed, also called as tool traverse speed, is one of the crucial parameters of FSW (Fig.2). The process temperature attained during welding increases with decreasing weld travel speed as well as increasing rotation speed of the tool. Thus, there exists an inverse relation between weld speed and heat generated. It is sufficient to increase rotation speed to increase weld temperature [6].

High welding speed has been proved to increase stress and wear on the tool. These can lead to an increased incidence of defects and require repairs or delivery of scrapped components. Hence, the optimum welding speed is therefore not normally the fastest possible speed.

3.3 Tool rotational speed

Another process parameter of FSW is the rotation speed of the tool. It is directly related to the increase in processing temperature. The increase of the rotation speed results in a higher processing speed and need higher cooling rates.

3.4 Plunge depth and force

Heel plunge depth corresponds to the distance the heel extends into the weld metal (Fig.2). The axial force is the force applied to the workpiece

along the axis of tool rotation. The downward force applied ensures the continuous contact between the shoulder and the workpiece surface to generate heat from the friction of these two surfaces. This force is necessary to ensure a constant heel plunge depth and a good weld. The axial force is directly related to the plunge depth, the deeper the heel plunge depth the higher will be the axial force.

3.5 Tool tilt angle

Tilt angle is the angle between the centerline (Fig.2) of the tool and a line perpendicular to the surface of the workpiece. A featureless shoulder usually employs a tilt angle, leaning backward in respect of the welding path, which means there is more room in front of the tool, and the back of the tool does the forging of material behind the pin.

3.5 Dwell time

The time period during which the stationary rotating tools preheats the material to achieve sufficient temperature ahead of the tool is called Dwell time. This is also equivalent to the time period of the tool into the workpiece.

4. FSW of dissimilar metals alloys

The joining of dissimilar metals by FSW is a growing area of concern because of the limitations. The common setbacks that need to be addressed in FSW of joining dissimilar metals are following:

4.1 Heat generation and temperature distribution

The analytical estimation of heat generation at the tool-workpiece interface in conventional welding is relatively easier because of the presence of only one type of material in contact with the tool. However, things become quite complicated when it comes to heat generation and temperature distribution in dissimilar FSW. Two different materials, have different thermal properties, coefficient of friction, and softening characteristics all these affect heat generation and the temperature distribution in the workpieces. In dissimilar material joining, the presence of changing thermal field induces a narrow temperature gradient in low thermal diffusivity material that would result in a lack of bonding and defects at the weld root.

4.2 Formation of intermetallic compounds

In conventional fusion welding of dissimilar metals, the formation of the intermetallic compound leads to loss of joint strength and integrity. The

factors contributing to the formation of intermetallic compounds are weld parameters and temperature. On having stringent control over the weld parameters, the formation of compounds can be minimized though it is not eliminated. Further, such formation in FSW is minimal which makes FSW joints with higher mechanical strength.

4.3 MATERIAL FLOW IN WELDING ZONE

The material flow during FSW is separated into two kinds of flow as given below.

- **Material flow due to pin:** layer by layer
- **Material flow due to shoulder:** material from retreating side(RS) is transferred through the shoulder surface at the top of the advancing side (AS)[7].

Fig. 5 Material Flow in FSW

Fig. 5 is the representation of material flow in FSW with the legend (arrow) explanation as follows:

- A part of the material is transferred from RS to AS (red arrows).
- A volume of material from the upper part of AS and down from the left area of the flow arm is deposited to the right part of the extrusion zone (at AS) and to the middle of the weld nugget (white arrows).
- Another volume of material of the extrusion zone at RS is shifted downwards and to the rear (yellow arrows).
- The down part of the weld nugget is composed of the vortex zone (blue arrows).

4.4 Weld Zones in FSW

Unlike another welding process, FSW has few additional zones in the weld as listed below:

- Pre-heat

- Initial deformation
- Extrusion
- Forging
- Cooldown

Fig. 6 Zones of FSW

- The heat produced from the rotating motion of the tool preheats the area in front of the tool.
- The rotational motion of the tool creates the initial deformation zone.
- In this zone, the metal is forced upward into the shoulder and then down into the extrusion zone.
- In the extrusion zone, the metal front is moved around the pin tool to the exit wake of the weld in the cavity being vacated by the pin as it moves forward.
- The back part of the shoulder passes over the metal that exits from the extrusion zone and forges it, ensuring the welding.
- Then, the metal cools down.

5. Properties of FSW quality

There are various qualifying parameters to quantify welded joints. Most often they are the prerequisite for all types of weld joints. The weld quality parameters are classified as

5.1 Mechanical properties

The mechanical properties of the weld are crucial in arriving at the resultant weld strength. Some of the common mechanical properties that determine the weld quality are Tensile strength, Strength/weight ratio, Elastic modulus, Shear strength, Impact strength, percentage elongation, Wear, Corrosive behavior, fracture characteristics, Fatigue, etc.

5.2 Microstructural properties

Every FSW process parameter considered during welding has a significant impact on the final microstructure[5]. Microstructural evaluation reveals the changes happening within the weld zone and the formation of intermetallic compounds. Some of them are Scanning Electron Microscopy (SEM), TEM, Dispersive X-ray analysis techniques which include EDX & XRD, EBSD, Optical microscopy etc[8].

5.3 Thermal properties

In addition to the mechanical and microstructural properties of welded joints, the thermal behavior of the weld joint is yet another property influenced by the FSW process parameters. In the case of dissimilar alloys, the role of temperature is crucial as it determines the formation and thickness of intermetallic compounds. Some of the common thermal analysis methods like Thermogravimetric analysis, Differential scanning calorimetry, Thermomechanical analysis, etc. can be used to understand the behavior of the materials /metals.

6. FRICTION STIR WELDING OF ALUMINIUM AND STEEL

6.1 Materials

The materials considered for comparing the FSW weld properties are plates of 2-mm-thick

- SS400 mild steel (hereafter, Fe) and
- A5083 (Al-0.5 Mg-0.5 Mn wt-%) aluminum alloy (hereafter, Al).

The material properties considered in this article are the ultimate tensile strength of the A5083 and SS400 which are 275 MPa and 455 MPa respectively. The shape and size of the material taken for the weld are rectangles with size 140x40x2(all dimensions are in mm)[9].

6.2 Method

The chosen material was cleaned with fine-grit emery paper to remove dust and then mounted on the jig with the weld face of length 140mm facing one another and clamped firmly. The tool steel (SKH57) was used to make FSW tool with a 15 mm diameter shoulder and unthreaded pin of 1.9 mm long and 2 mm diameter, as shown in Fig. 7.

The rotating speed of the FSW tool was in the range 100 – 1250 rpm with 25 mm/min transverse speed[10]. The Al plate was located on the retreating side as shown in Fig. 7. After the rotating pin was inserted into the Al plate, the pin was thrust toward the Fe faying surface by the distances of –0.2 mm to 2 mm (zero is at the position where the pin side face is located just at the Fe faying surface, and the offset is defined as shown in Fig. 7b).

Studies were also performed with weaving pattern assigned to tool path for better weld quality [11-18]

6.3 Testing of Weld Specimens

1. Tensile test was employed to estimate the tensile strength of the joints and the fracture path. The tensile test specimens perpendicular to the weld interface were machined from the welds. While machining, it was made to have welded area at the center of the tensile specimen.
2. Metallographic samples were produced from the welds and etched with only an etchant of 3%. Etched samples were examined using an optical microscope and scanning electron microscope (SEM) with X-ray and energy-dispersive spectroscopy (EDS).

Fig. 7. FSW of Fe and Al

A bird's-eye view of the method and a view of the cross-section perpendicular to a weld interface are depicted in Fig. 7. While welding by FSW, the rotating tool pin is pushed toward the faying surface of the hard material – Steel which removes the oxide film from the material surface by the rubbing action of the tool.

Aluminum, which is in a fluid-like plastic state due to the heat generated by the friction of the rotating tool shoulder, adheres to the activated faying surface of the steel so that joining between steel and aluminum is achieved. In this process, the tool wear is minimal due to the fact that the rotating pin is plunged into the softer aluminum and does not come in contact with the steel.

Welding by FSW is ordinarily completed through stirring by a rotating pin inserted around the center of the weld interface of butted base plates. A preliminary experiment proved that when the rotating pin was inserted around the center of the weld interface between the steel plate and the aluminum alloy plate, welding could not be achieved because of excessive wear of the rotating pin in a short duration. The wear caused insufficient stirring between the aluminum alloy and the steel.

6.4 Results and discussion

• Effect of Pin Rotation Speed on Joint Tensile Strength

Fig. 8 Tensile strength Vs Pin rotation speed in FSW

The rotation speed of the pin is significant in heat generation. At 100 rpm the heat generation was minimal and unable to plasticize even soft metal Al. Hence, there was an incomplete fusion between Fe and Al, so the tensile strength of these specimens was low. In contrast to the above and on rising pin rpm to 250, complete mixing of metal is possible offering maximum tensile strength of 24 MPa which is 86% of the base metal.

With the further rise in pin rpm to 500, the surface morphology of the weld was similar to that of 250 rpm; however, the joint strength was not much appreciable than at 250 rpm. At 1250 rpm, the joint failed much earlier than other rotational speeds

attributed to the effect of weld zone oxidation and incomplete weld.

The fracture surface appeared to be heavily oxidized and appeared to be burned. Thus the above results show to highlight the optimum tool rpm for this combination of Al- Fe joint by FSW is 250 rpm.

• The Effect of Pin Offset on Joint Tensile Strength

The effect of pin offset on the tensile strength of a FSW joint of Al- Fe metal is shown in Fig. 9. The experimental condition considered for the evaluation are pin rotation speed – 250 rpm and transverse velocity – 25 mm/min. The pin face contact wrt line of joint may give positive or negative offset. For positive offset, not more than 0.2 mm exhibited higher tensile strength and any variation from 0.2 mm either positive or negative there exist strength degradation.

Fig. 9 Tensile Strength Vs Pin Offset in FSW

• The Effect of Rotating Pin Diameter on Joint Strength

Fig. 10 Tensile Strength Vs Pin dia in FSW

Most often, a rotating pin of a diameter of 2-mm was used to make a joint. In this section, the effects of various pin diameters on joint strength are examined. Joints were made using pins of 1, 3, and 4 mm

diameter under the welding conditions of 0.2-mm pin offset, 250-rpm pin rotation speed, and 25-mm/min welding speed. A pin of 1 mm diameter wore out in such a short duration that a sound joint could not be produced. The tensile strength of the joint made with a pin of 3 or 4 mm diameter was similar to those made using a 2-mm-diameter pin. It appears that rotating pin diameter has little effect on joint strength(Fig. 10).

• The Effect of direction of pin rotation

The effect of pin rotation direction on joint performance was also examined by many researchers. In this work, the pin rotation direction was reversed in comparison to other FSW. On having counterclockwise pin rotation direction, the position of Al was on the advancing side of the joint.

The weld parameters taken in this work are 2 mm pin diameter, 250 rpm pin rotation speed and 25 mm/min welding. It appears from Fig.11 a and b, that welding was successfully achieved. However, welding was restricted to the top surface and showed little bonding within the plate.

Fig. 11 Rotation direction of pin in FSW

CONCLUSION:

In this study, the effects of pin rotation speed and pin offset toward the steel faying surface on the tensile strength of a joint were reviewed and the following results are arrived.

➤ An optimum rotation speed for the pin would exist to make a sound joint. At lower tool rpm, heat generation is high that leading to pin wear however, oxidation is expected at a higher rotation speed.

➤ Rotating pin position helps to activate the faying surface of the metal and enables a joint to be produced.

➤ Minimum pin offset toward hard material results in reduced scattering in soft alloy with minimal voids and enhanced joint tensile strength.

➤ Higher weld zone temperature results in Intermetallic compounds which deteriorates the weld strength.

➤ A minimum pin size was required to produce a weld. Pins with very small diameters ($\leq 1\text{mm}$) could not support welding and Pins with 2 mm has the same tensile strength. This opens up the need of a parametric study of the Pin size effect on the mechanical strength of FSW joints.

➤ Sound weld joints are also controlled by effective selection of pin rotation direction.

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