50 nm THICK ALUMINUM NITRIDE PIEZOELECTRIC NANO-PLATE RESONANT THERMAL DETECTORS

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ABSTRACT

This paper reports on the first demonstration of ultra-fast (thermal time constant, $\tau < 10 \mu s$) and high resolution (noise equivalent power, $NEP \sim 4 \text{ nW/Hz}^{1/2}$) thermal detectors based on 50 nm thick Aluminum Nitride (AlN) piezoelectric resonant nano-plates. Efficient piezoelectric transduction of a high frequency ($\sim 1 \text{ GHz}$) lateral-extensional mode of vibration in a 50 nm thick AlN nano-plate is demonstrated for the first time and exploited for the implementation of the smallest volume ($\sim 87 \mu m^3$) laterally vibrating piezoelectric NEMS resonators reported to date. The effects of volume scaling on quality factor, Q , temperature coefficient of frequency, TCF , and associated detector NEP and τ are experimentally investigated.

INTRODUCTION

One of the most important requirements for the implementation of a high resolution and simultaneously ultra-fast MEMS/NEMS resonant infrared (IR) detector is the scaling of the resonator thickness [1]. In fact, the scaling of the device thickness, t , while maintaining the resonator static electrical capacitance, C_0 , constant to a value larger than the substrate parasitic capacitance, inevitably yields an improved IR detector figure of merit: $FoM = 1/(NEP \cdot \tau) \propto (\eta \cdot TCF \cdot Q)/(C_0 \cdot t^2)$, where η is the IR absorption coefficient of the structure. AlN resonant thermal detectors as thin as 500 nm have been recently demonstrated showing excellent thermal detection capabilities ($NEP \sim 0.4 \text{ nW/Hz}^{1/2}$, $\tau \sim 20 \text{ ms}$, $FoM \sim 125 \text{ nW}^{-1} s^{3/2}$) [2]. Nevertheless, despite such a high performance (comparable to the one of other existing uncooled IR detector technologies) the size of the demonstrated MEMS resonant IR detectors is ~ 1 order of magnitude larger than the one of commercially available microbolometers. This relatively large detector size has fundamentally prevented this technology from addressing the growing needs of small pixel size IR cameras for both military and civilian applications. In this work, we show that, by scaling the resonator thickness to 50 nm it is possible to implement IR detectors with reduced lateral dimensions (down to $32 \times 28 \mu m^2$), comparable to the ones of commercially available microbolometers, and characterized by a $FoM \sim 2$ orders of magnitude higher than what previously achieved by MEMS/NEMS resonant thermal detector technologies.

EXPERIMENTAL RESULTS

In this work an ultra-thin (50 nm) and high quality ($FWHM < 3^\circ$) AlN piezoelectric layer is employed to form the resonant bodies of lateral-extensional mode resonators (Fig. 1) with 5 different lateral dimensions ranging from $60 \mu m$ to $28 \mu m$ (Fig. 2). Moreover, thicker devices (200 nm and 500 nm) for each size are built as references to prove the effectiveness of volume scaling in improving device performance. The electromechanical performance of both the 50 nm thick devices and reference devices were characterized (Fig. 3, 4), demonstrating that the scaling of the device thickness down to 50 nm allows to maintain sufficiently high values of device capacitance (low impedance) while simultaneously guaranteeing the achievement of high electromechanical performance ($f \cdot Q \sim 10^{12}$ and $k_t^2 \cdot Q \sim 10$) comparable to that of $10X$ thicker devices. Furthermore, the experiments demonstrate that the use of a 50 nm thick AlN layer

yields higher Q values when the lateral dimensions of the devices are reduced below $50 \mu m$.

Figure 1: 3D schematic representation of the AlN nano-plate resonant thermal detector.

Figure 2: (a) to (c) SEM images of fabricated 50 nm AlN nano plate resonators with various lateral dimensions. Totally 5 different sizes were designed ($60 \times 68 \mu m^2$, $59 \times 52 \mu m^2$, $50 \times 44 \mu m^2$, $41 \times 36 \mu m^2$ and $28 \times 32 \mu m^2$). The pitch, W_0 , of the top IDE is fixed at $4 \mu m$ for all devices. $t_{Al} = 50 \text{ nm}$, $t_{Pt} = 25/50/100 \text{ nm}$ for 50/200/500 nm AlN and $t_{Au} = 100 \text{ nm}$. (d) A cross sectional view highlighting the 50 nm AlN thin film deposited on the Si substrate.

Figure 3: Q factor values extracted from MBVD fitting of the fabricated scaled devices with various thicknesses of the AlN nano plate. For lateral dimensions below $50 \mu m$, the 50 nm thick devices show higher Q than the thicker ones. Low device capacitance and spurious modes prevent measurements of Q values for the smallest 500 nm and 200 nm AlN devices. The extracted k_t^2 (without de-embedding) of these devices varies between 1.1% and 0.7%.

The thermal capacitances of the fabricated devices were estimated based on their geometries and material properties (Fig. 4) showing an ultra-low thermal time constant, $\tau \sim 2 \mu\text{s}$, for the smallest 50 nm thick device. The thermal resistances, R_{th} of the 50 nm, 200 nm and 500 nm thick devices were estimated based on their anchor geometries and material composition (not optimized in this work) and found to be $\sim 1 \times 10^4 \text{ K/W}$, $0.6 \times 10^4 \text{ K/W}$ and $0.4 \times 10^4 \text{ K/W}$, respectively. The TCF of devices with three different thicknesses were characterized (Fig. 5), showing a high temperature sensitivity $\sim 52.5 \text{ ppm/K}$ for the 50 nm devices (due to the more significant contribution of the metal electrodes characterized by a relatively large temperature coefficient of Young's modulus). These unique features were exploited for the first experimental demonstration of ultra-fast and high resolution AlN NEMS resonant IR detectors. The detectors were characterized using a Pendar Technologies 5 μm quantum cascade laser and the experimental setup shown in Fig. 6. The frequency response to a modulated IR radiation of a 50 nm device was measured and compared to that of a 200 nm one (Fig. 7). The intrinsic absorption peaks of both the 50 nm and the 200 nm AlN devices are located at wavelengths much shorter than 5 μm [3]. Therefore, they are both characterized by small and comparable values of IR absorptance, η , at $\sim 5 \mu\text{m}$. The measurement results show a 2X improvement in responsivity ($S \propto \eta R_{th} \text{ TCF}$) for the 50 nm device in agreement with the analytical predictions. The frequency noise spectral densities, f_n , of the two devices were extracted from the measurements and the NEP values were then calculated ($\text{NEP} = f_n/S$, assuming $\eta = 1$) to be $\sim 4 \text{ nW/Hz}^{1/2}$ for the 50 nm device and $\sim 6 \text{ nW/Hz}^{1/2}$ for the 200 nm one. It is worth noting that, these values can be easily reduced to the pW range by optimizing the anchor design [2]. The response times of the two devices were estimated ($\tau = C_{th} R_{th}$) to be $\sim 10 \mu\text{s}$ for the 50 nm device and $\sim 16 \mu\text{s}$ for the 200 nm one. These experimental results demonstrate that the scaling of the resonator thickness enables the implementation of resonant IR detectors with largely improved detection capability ($\text{FoM} \sim 2.5 \times 10^4 \text{ nW}^{-1} \text{ s}^{-3/2}$), smaller form factor and reduced electrical impedance.

Figure 4: Measured device capacitances and estimated thermal capacitances as functions of the device area. When the device capacitance is smaller than 100 fF, it becomes comparable to the substrate parasitic capacitance deteriorating the effective electromechanical coupling of the resonant element (higher electrical impedance and insertion loss). Thermal capacitances are estimated based on the geometry and material properties of each device. C_{th} as low as 0.2 nJ/K is estimated for the smallest 50 nm device, rendering an ultra-low thermal time constant of $\sim 2 \mu\text{s}$.

Figure 5: Measured TCF for devices with different thicknesses.

Figure 6: Experimental setup for infrared sensing measurements.

Figure 7: Measured frequency responses of a 50 nm device and a 200 nm reference with same lateral dimensions ($60 \times 68 \mu\text{m}^2$) when exposed to a 5 μm IR radiation modulated at 1 Hz by a chopper.

REFERENCES

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