Adsorption of Nitenpyram and *p*-Cresol from Water in Binary Components System with Modified Resin with Tannic Acid

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(Received: 23 April 2013;

Accepted: 20 November 2013)

AJC-14423

The adsorption behaviour of nitenpyram and *p*-cresol in water onto the resin modified with tannic acid based was investigated by static adsorption experiments at different temperature (288, 303, 318 K) in single component and binary components system. The adsorption capacities and adsorption selectivity for nitenpyram and *p*-cresol in water were tested. The results show that the adsorption is fitted better by Freundlich model than Langmuir model. The adsorption of nitenpyram on the resin modified with tannic acid was an endothermic process by the positive adsorption enthalpy and an exothermic process of *p*-cresol with the negative adsorption enthalpy. The resin had better absorbability for nitenpyram than for *p*-cresol and the adsorption selectivity of nitenpyram was larger than one. Gibbs free energy, enthalpy change and entropy change had changed in binary components system, to demonstrate the existence of the cooperative effect. A high removal rate of 48.55-94.26 % was obtained for nitenpyram and 28.93-71.71 % for *p*-cresol in single component system, which was lower in binary components system. But in binary components system of the same initial concentration of nitenpyram and *p*-cresol, when the equilibrium concentration was higher, the cooperative adsorption existed, which may be due to the hydrogen bonding or weak acid-base interaction between nitenpyram and *p*-cresol. The competitive adsorption existed, because the adsorption of nitenpyram onto the resin had just smaller change in the presence of *p*-cresol, but the adsorption of *p*-cresol was weakened in the presence of nitenpyram.

Key Words: Adsorption resin, Nitenpyram, *p*-Cresol, Binary components system, Cooperative adsorption.

INTRODUCTION

Pesticides are widely used to control the plant pests¹. Nitenpyram (Fig. 1) is a new nicotine insecticide with high and fast effectiveness, destroys insects widely, has a persistent efficiency period for 50 days and better solubility under room temperature². There is a serious need for the high-tech about the economic, efficient, feasible wastewater treatment, to protect the environment. Resin adsorption is widely used in wastewater treatment³, which makes resin adsorption technology has irreplaceable characteristics because of the designability and selectivity of resin's chemical or physical structures on practical application^{4,5}. It offers most effective technology in the field of removal of organic substance. Compared with the single component adsorption, the adsorption rule is complicated and few papers were reported in binary component system in aqueous solution⁶⁻¹¹. The paper focuses on the adsorption of nitenpyram in aqueous solution on the resin modified with tannic acid¹² and the adsorption behaviour of bicomponent pollutants coexisting in water, modified adsorption resin as adsorbent, nitenpyram (Fig. 1) and *p*-cresol as adsorbates through static adsorption. A thermodynamical study is also made.

Fig. 1. Structure of nitenpyram

EXPERIMENTAL

Methanol is of G.R. grade. Both *p*-cresol and nitenpyram are of A.R. grade and the resin of is modified with tannic acid based on NDA150¹².

Static adsorption experiment: A bottle point isotherm procedure was used to conduct all the equilibrium studies in single component system. 0.1 g of the resin was directly weighed accurately. The adsorbents were contacted, in 250 mL stoppered conical flasks, with 100 mL of *p*-cresol or nitenpyram solution of certain concentration (C_0 , mg/L) ranging from 100 to 500 mg/L. The flasks were completely sealed and then placed in an incubator shaker at different temperatures (288, 303, 318 K) until equilibrium was achieved.

Experiments of binary solute isotherms were performed according to the above procedure. The main differences were that the initial concentrations of nitenpyram and *p*-cresol were equal to each other in the range of 50-250 mg/L. Other binary solute isotherms were also performed following the above procedure. The main differences were that the initial concentrations of nitenpyram were constant at 300 mg/L and those of *p*-cresol were in the range of 100-500 mg/L. Conversely, the initial concentrations of *p*-cresol were constant at 300 mg/L.

RESULTS AND DISCUSSION

Static adsorption in single component system

Static adsorption of nitenpyram and *p*-cresol in single component system: Equilibrium adsorption isotherms of the single solute of nitenpyram and *p*-cresol onto the resin are presented in Fig. 2. The isotherm corresponding to higher temperature lies above, which shows the endothermic process, with higher adsorption amounts at lower temperature for nitenpyram, but for *p*-cresol it is the exothermic process.

Fig. 2. Equilibrium adsorption isotherms of nitenpyram and *p*-cresol in single component system on the resin at 288-318 K

A high removal rate of 48.55-94.26 % was obtained for nitenpyram studied, as shown in Fig. 3, which may be attributed to the relatively stronger interaction between the acid groups on the adsorbent and the basic groups of the solute at the adsorption process. But with the increasing adsorption capacities there are some shields for the limited amount of adsorption sites or basic functional groups for the higher removal rate on the lower concentration and the higher temperature. But removal efficiency (28.93-71.71 %) was obtained for *p*-cresol studied from Fig. 3, which results from initial higher concentration.

Fig. 3. Removal rate of nitenpyram or *p*-cresol at different temperatures and initial solute concentrations in single component system

Many theories, used to model the adsorption process with varying degrees of success, have been proposed to explain the adsorption phenomenon and to describe the adsorption isotherm relationships. Among them the Langmuir and Freundlich models have been widely used and their linear forms are given below respectively¹³.

$$\text{Langmuir model: } C_e/Q_e = C_e/M + 1/(MK_L) \quad (1)$$

$$\text{Freundlich model: } \log Q_e = \log K_f + 1/n \log C_e \quad (2)$$

where M , K_L , K_f and n are characteristic constants. The Langmuir constant M (mmol/g) is the maximum amount per

weight of adsorbent to form a complete monolayer on the surface bound and K_L (L/g) is a constant related to the affinity of the binding sites. The Freundlich coefficient K_f (L/mmol) is an index of the sorption capacity of the resins and the Freundlich exponent ' n ' (dimensionless) denotes the heterogeneity of the surface and the intensity of adsorption.

By a non-linear least square routine, the regression equations corresponding to the above isotherms can be obtained and their constants along with the correlation coefficients r are summarized in Table-1. The results clearly show that the adsorption data for the studied adsorption systems of nitenpyram fits better to the Freundlich model and to *p*-cresol, both.

As seen from the values of M and K_L in Table-1, the capacity of nitenpyram increases with increasing initial lead concentration, temperature for the interaction between basic groups of nitenpyram and acid groups on the resin modified with tannic acid, maybe share electrons. Conversely, the capacity of *p*-cresol decreases with the increasing temperature, indicating the predominant phenomena of "sorbent-motivated" effects caused mainly by the electrostatic interaction and ion change which are exothermic interactions. And the constant ' n ' is always more than 1 in our study range, indicating a favourable type adsorption.

Thermodynamics: Thermodynamic parameters such as Gibbs free energy (ΔG), enthalpy change (ΔH) and entropy change (ΔS) for the adsorption of nitenpyram and *p*-cresol onto the resin are given in Table-2.

ΔG is calculated according to eqn. 3 the data onto the resin better fitted to the Freundlich model¹⁶. Thus, the calculation of ΔG in binary components system is the same as in single component system.

$$\Delta G = -nRT \quad (3)$$

where n is the Freundlich model characteristic constant, R is the gas constant (kJ/mol K) and T is the absolute temperature (K).

The following Gibbs-Helmholtz equation can be obtained to describe the relation between ΔG and the other two thermodynamic parameters.

$$\Delta G = \Delta H - T\Delta S \quad (4)$$

Then, ΔH can be calculated respectively from the van't Hoff equation.

$$\ln (Q_e/C_e) = -\Delta H/RT + \ln K_0 \quad (5)$$

The estimated enthalpy of adsorption of nitenpyram is positive, indicating the adsorption process is an endothermic one. The enthalpy of *p*-cresol is negative, an exothermic process. Both are low and in the range of 10-40 kJ/mol where physical adsorption is expected to be the dominant mechanism.

It is well known that the free energy change value for a physical sorption, which is in the range of -20 to 0 kJ/mol. A chemical sorption process is in the range of -400 to -50 kJ/mol. The free energy changes are small (Table-2), further confirming the physical character of the adsorption. As expected they are negative in all cases because the solute is more concentrated on the surface of the adsorbents than in the bulk solutions. The magnitude of the free energy changes indicates the stronger adsorption force between the resin and nitenpyram for the partially polar groups in its net work, with the results of equilibrium static adsorption.

The negative values of the adsorption entropy are consistent with the restricted mobility of the adsorbed *p*-cresol molecules compared with those in solution. Thus a more ordered arrangement of solute molecules for *p*-cresol is formed on the surface of the resin modified with tannic acid. But for nitenpyram the values of the adsorption entropy is positive, so the adsorption is driven by enthalpy and an irreversible process.

Static adsorption in binary components system

Same initial concentration of nitenpyram and *p*-cresol in binary components system: Equilibrium adsorption isotherms of nitenpyram and *p*-cresol onto the resin in binary components system are presented in Fig. 4. For nitenpyram, temperature has little effect on the attachment. It shows good treatment efficiency in Fig. 5.

Higher removal efficiency rate was obtained for nitenpyram (Fig. 5), in the range of 55.16-98.47 %, but for *p*-cresol just in

TABLE-1
FITTED RESULTS FOR LANGMUIR AND FREUNDLICH MODELS IN SINGLE COMPONENT SYSTEM

Regression Requisitions	Parameters	Nitenpyram			<i>p</i> -Cresol		
		288 K	303 K	318 K	288 K	303 K	318 K
Langmuir	M	10.787	19.157	26.882	3.769	2.857	2.119
	K_L	0.073	0.043	0.032	0.520	0.699	0.740
	r	0.944	0.949	0.949	0.995	0.998	0.994
Freundlich	K_f	0.883	0.954	1.069	1.187	1.084	0.834
	n	2.869	3.311	3.340	2.406	2.206	2.325
	r	0.980	0.985	0.985	0.996	0.998	0.994

TABLE-2
THERMODYNAMIC PARAMETERS FOR ADSORPTION OF NITENPRYRAM
OR *p*-Cresol ONTO THE RESIN IN SINGLE COMPONENT SYSTEM

Adsorbate	q_e (mmol/g)	Temperature (K)	ΔH (kJ/mol)	ΔS (J/mol K)	ΔG (kJ/mol)
Nitenpyram	1.0	288	14.616	74.604	-6.870
	1.0	303	14.616	75.766	-8.341
	1.0	318	14.616	73.729	-8.830
<i>p</i> -Cresol	1.0	288	-20.974	-52.823	-5.761
	1.0	303	-20.974	-50.881	-5.557
	1.0	318	-20.974	-46.616	-6.150

Fig. 4. Equilibrium adsorption isotherms of nitenpyram or *p*-cresol in binary components system

Fig. 5. Removal rate of nitenpyram or *p*-cresol at different initial solute concentrations in binary components system

the range of 38.68-72 %. Compared with the results of the single component system, the capacity of the resin has been improved better in binary components system.

Contrasting Fig. 6 of the binary components system with Fig. 2, the adsorption capacity of *p*-cresol and nitenpyram in binary components system were more than the adsorption capacity in single component system (nitenpyram or *p*-cresol) on the resin at the same higher equilibrium concentration, which would be due to the cooperative effect primarily arisen from the acid-base interaction between nitenpyram and *p*-cresol; when the equilibrium concentration (*e.g.*, 0.4 mmol L⁻¹) was lower in Fig. 6, the capacity was less than it in Fig. 2, because of the competition on the adsorption locus, these molecules were organized in the arrangement out of disorder. From Fig. 4 and Table-3, in binary components system the equilibrium adsorption isotherms could also be fitted by Freundlich model better than Langmuir model, the values of *n* and *K_f* was lower than them in Table-1, *r* was greater than 0.988 and Fig. 5 also provided data supporting for the cooperative effect, with higher removal rate.

Fig. 6. Equilibrium adsorption isotherms of both nitenpyram and *p*-cresol on ZHP02 in binary components system

Thermodynamic parameters such as Gibbs free energy (ΔG), enthalpy change (ΔH) and entropy change (ΔS) for the adsorption of nitenpyram and *p*-cresol onto the resin with the same initial concentration of nitenpyram and *p*-cresol in binary components system are given in Table-4.

Comparing with the single component system (Table-2), in Table-4 there was variability in the thermodynamic parameters. The enthalpy change and Gibbs free energy of *p*-cresol decreased, but the enthalpy change of nitenpyram increased sharply. The entropy change of nitenpyram was more positive than it in Table-2, that randomness went up in the system, which could favour the adsorption process, further to demonstrate the existence of the cooperative effect.

Simultaneous adsorption in binary components system:

For further testifying the above predominant mechanism, the influence of initial concentration on the adsorption capacity was demonstrated in Fig. 7. In general, there was some drop in the adsorption amount of nitenpyram with the increasing initial concentration of *p*-cresol, but larger distinction for

TABLE-3
FITTED RESULTS FOR LANGMUIR AND FREUNDLICH MODELS IN BINARY COMPONENTS SYSTEM

Adsorbate	Temperature (K)	Langmuir			Freundlich		
		M	K_L	r	K_f	n	r
Nitenpyram	288	13.532	0.033	0.960	0.676	2.746	0.992
	303	28.985	0.016	0.971	0.773	3.134	0.998
	318	86.207	0.011	0.985	1.899	2.525	0.993
<i>p</i> -Cresol	288	3.211	0.482	0.992	1.121	1.702	0.988
	303	2.120	0.843	0.994	1.009	1.487	0.988
	318	1.726	0.709	0.980	0.741	1.564	0.988
Nitenpyram+ <i>p</i> -Cresol	288	4.427	0.432	0.987	1.356	1.902	0.993
	303	3.384	0.649	0.994	1.329	1.716	0.992
	318	2.973	0.609	0.984	1.115	1.756	0.994

TABLE-4
THERMODYNAMIC PARAMETERS FOR THE ADSORPTION OF NITENPRYRAM AND *p*-CRESOL ONTO THE RESIN ZHP02 WITH THE SAME INITIAL CONCENTRATION IN BINARY COMPONENTS SYSTEM

Adsorbate	Q_e (mmol/g)	Temperature (K)	ΔH (kJ/mol)	ΔS (J/mol K)	ΔG (kJ/mol)
Nitenpyram	1.0	288	65.523	250.3	-6.575
	1.0	303	65.523	242.3	-7.895
	1.0	318	65.523	227.0	-6.676
<i>p</i> -Cresol	1.0	288	-16.705	-43.85	-4.075
	1.0	303	-16.705	-42.77	-3.746
	1.0	318	-16.705	-39.53	-4.135
Nitenpyram + <i>p</i> -Cresol	1.0	288	-9.725	-17.95	-4.554
	1.0	303	-9.725	-17.83	-4.323
	1.0	318	-9.725	-15.98	-4.643

p-cresol with the increasing initial concentration of nitenpyram, competitive adsorption phenomenon existed. The change of nitenpyram' concentration had greater effect on the adsorption of *p*-cresol onto the resin modified with tannic acid, because of the stronger interaction between nitenpyram and the resin. Contrasting Fig. 8 with Fig. 2, the results were consistent with the data that the adsorption effect was related to temperature. The capacity of nitenpyram and *p*-cresol on the resin was in decreasing order, demonstrated the competition in the adsorption locus once again.

Selectivity index: Selectivity index often used to evaluate an adsorbent or an adsorptive process. If we define the distribution coefficient (solid-to-liquid) as:

$$D = Q_e/C_e \quad (6)$$

Fig. 7. Influence of initial concentration on the adsorption amount onto the resin from the binary components adsorptive environment

Fig. 8. Equilibrium adsorption isotherms of nitenpyram or *p*-cresol in binary components system with the constant initial concentration of another adsorbate at 300 mg/L

Then the selectivity index of the first component has the following form:

$$S_{1/2} = D_1/D_2 \quad (7)$$

D_1 and D_2 represent the distribution coefficient of two solutes respectively¹².

The selectivity indexes for the adsorption of nitenpyram onto the adsorbent tested are compared in Table-5, with 300 mg/L of *p*-cresol as the competitive component. It can be seen that the adsorption selectivity of nitenpyram on the resin is larger than one on higher temperature with lower concentrations, contributed to the larger difference in the adsorbent-solute interaction and solvent-solute interaction. Consequently, it is expected to apply the resin for the successful separation and recovery of nitenpyram from the water containing *p*-cresol. The proposed technique has its practicability.

TABLE-5
SELECTIVITY INDEX OF NITENPYRAM

C_0 of nitenpyram (mg/L)	Temperature (K)		
	288	303	318
100	2.030	3.302	4.400
200	1.492	2.145	3.299
300	1.085	1.405	2.218
400	0.932	1.201	1.792
500	0.836	1.033	1.579

Conclusion

The adsorption was fitted by Freundlich model better than Langmuir model, with higher linearity. The adsorption of

nitenpyram on the resin modified with tannic acid was an endothermic process by the positive adsorption enthalpy and an exothermic process of *p*-cresol with the negative adsorption enthalpy. The resin had better absorbability for nitenpyram than for *p*-cresol and the adsorption selectivity of nitenpyram was larger than one. Gibbs free energy, enthalpy change and entropy change had changed in binary components system, to demonstrate the existence of the cooperative effect. A high removal rate of 48.55-94.26 % was obtained for nitenpyram and 28.93-71.71 % for *p*-cresol in single component system, which was lower in binary components system. But in binary components system of the same initial concentration of nitenpyram and *p*-cresol, when the equilibrium concentration was higher, the cooperative adsorption existed, which may be due to the hydrogen bonding or weak acid-base interaction between nitenpyram and *p*-cresol. The competitive adsorption existed, because the adsorption of nitenpyram onto the resin had just smaller change in the presence of *p*-cresol, but the adsorption of *p*-cresol was weakened in the presence of nitenpyram.

ACKNOWLEDGEMENTS

The work was financially supported by the National Natural Science Foundation of China (21201147), sponsored by research fund of Jiangsu Provincial Key Laboratory of Coastal Wetland Bioresources and Environmental Protection (JLCBE12010).

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