

Supplementary Data

BaY₁₆Si₄O₃₃ containing Ba(SiO₄)₄ orthosilicates

Shuto Motozawa,^{1,2} Hiromitsu Kimura,³ Junichi Takahashi,¹ Rayko Simura¹ and Hisanori Yamane^{1*}

¹ Institute of Multidisciplinary Research for Advanced Materials, Tohoku University, Katahira 2-1-1 Aoba-ku, Sendai 980-8577, Japan

² Department of Metallurgy, Materials Science and Materials Processing, Graduate School of Engineering, Tohoku University, 6-6-4 Aramaki Aza Aoba, Aoba-ku, Sendai 980-8579, Japan

³ Science & Innovation Center, Inorganic Materials Laboratory, Mitsubishi Chemical Corporation, 1000 Kamoshida-cho, Aoba-ku, Yokohama-shi, Kanagawa 227-8502, Japan

*Correspondence e-mail: hisanori.yamane.a1@tohoku.ac.jp

Fig. S1. Relative dielectric constant (ϵ_r) and dielectric loss ($\tan \delta$) of BaY₁₆Si₄O₃₃ ceramics at 298 K as functions of frequency (f).

Fig. S2. Relative dielectric constant (ϵ_r) and dielectric loss ($\tan \delta$) of BaY₁₆Si₄O₃₃ ceramics at 1 MHz as function of temperature.

Fig. S3. Thermal expansion of BaY₁₆Si₄O₃₃ ceramic as function of temperature.

Fig. S4. Experimental (dot) and calculated (solid line) profiles obtained from Rietveld refinement of X-ray powder diffraction data for BaY₁₆Si₄O₃₃ at 298 K. The difference profile (bottom) is on the same scale. Vertical ticks indicate the calculated positions of all possible Bragg reflections for BaY₁₆Si₄O₃₃.

Table S1 Crystallographic data for BaY₁₆Si₄O₃₃, as derived from Rietveld refinement of powder XRD data.

Table S2 Atomic coordinates and overall isotropic displacement parameter (U_{iso}), as derived from Rietveld refinement of powder XRD data for BaY₁₆Si₄O₃₃.

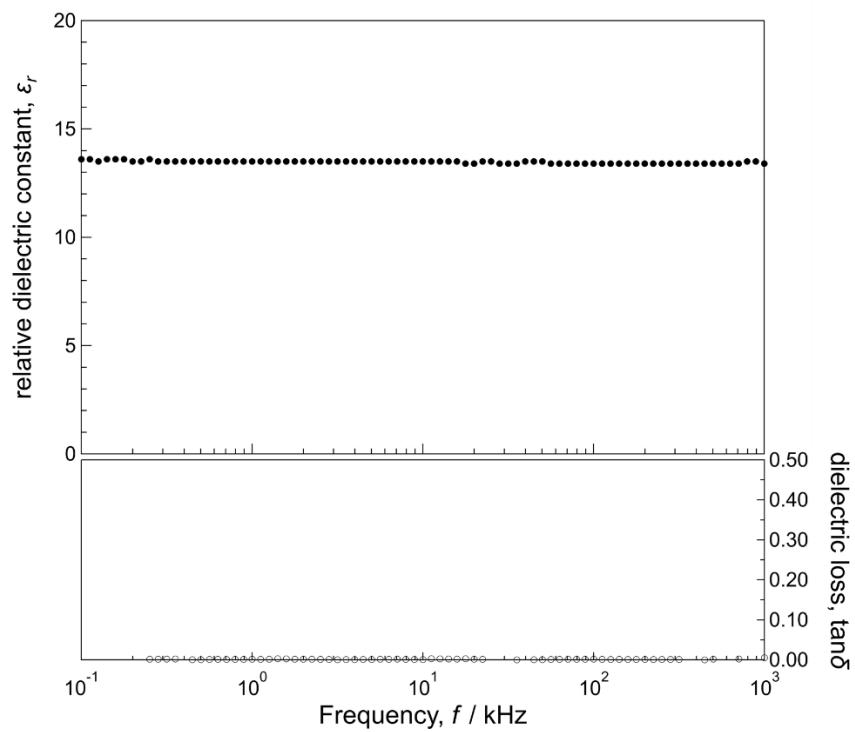


Fig. S1. Relative dielectric constant (ϵ_r) and dielectric loss ($\tan \delta$) of $\text{BaY}_{16}\text{Si}_4\text{O}_{33}$ ceramics at 298 K as functions of frequency (f).

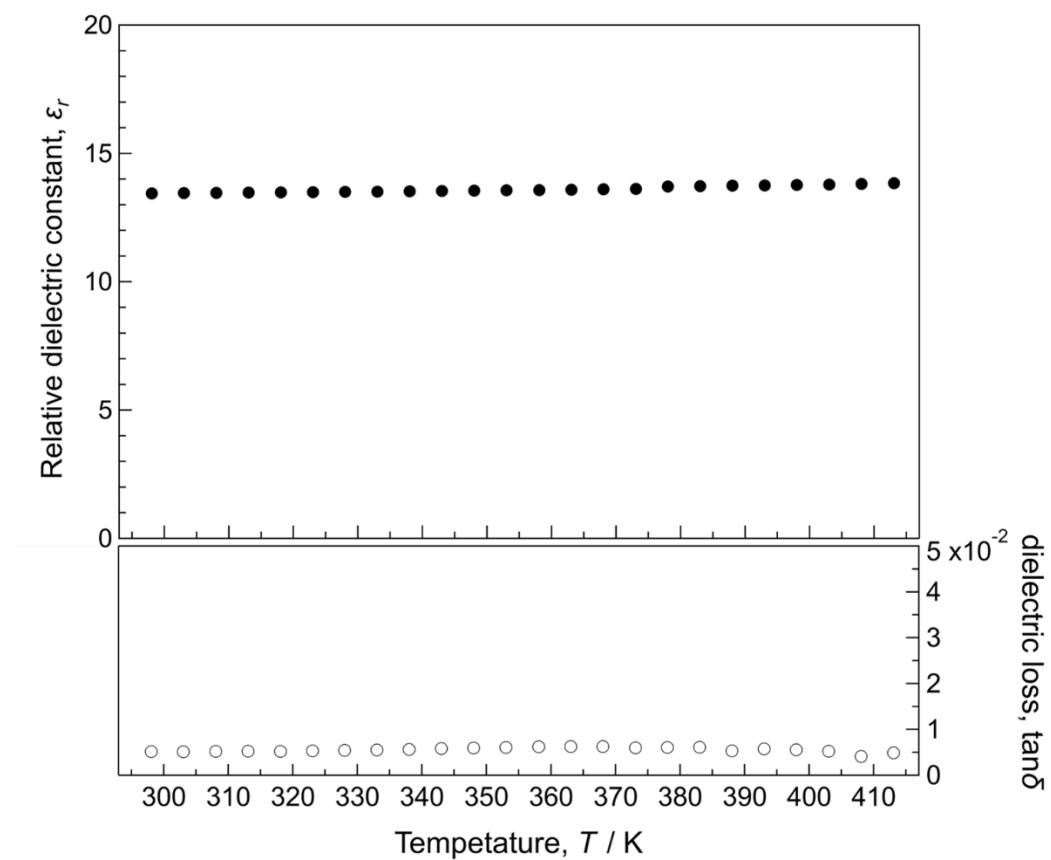


Fig. S2. Relative dielectric constant (ϵ_r) and dielectric loss ($\tan\delta$) of $\text{BaY}_{16}\text{Si}_4\text{O}_{33}$ ceramics at 1 MHz as function of temperature.

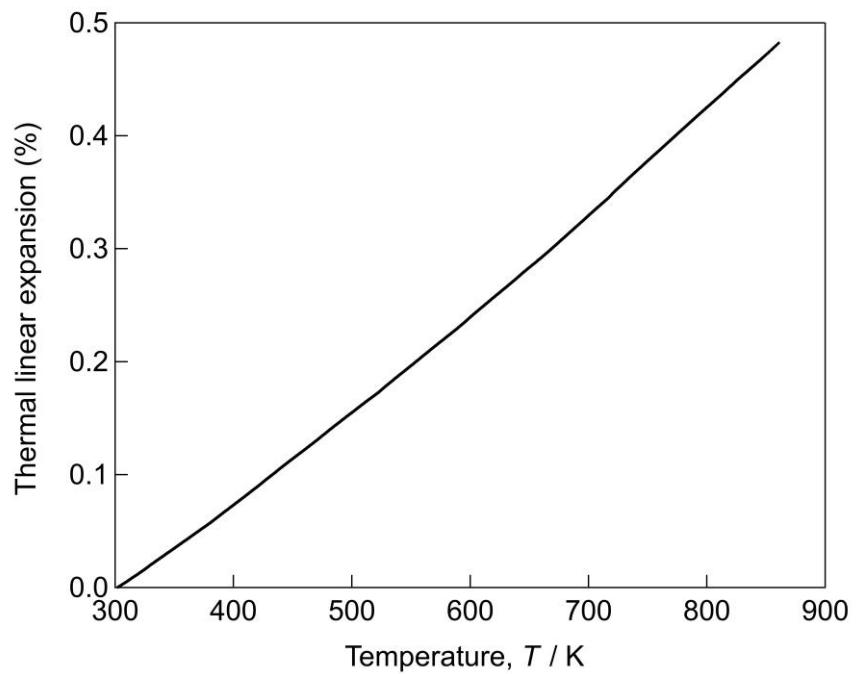


Fig. S3. Thermal expansion of $\text{BaY}_{16}\text{Si}_4\text{O}_{33}$ ceramic as function of temperature.

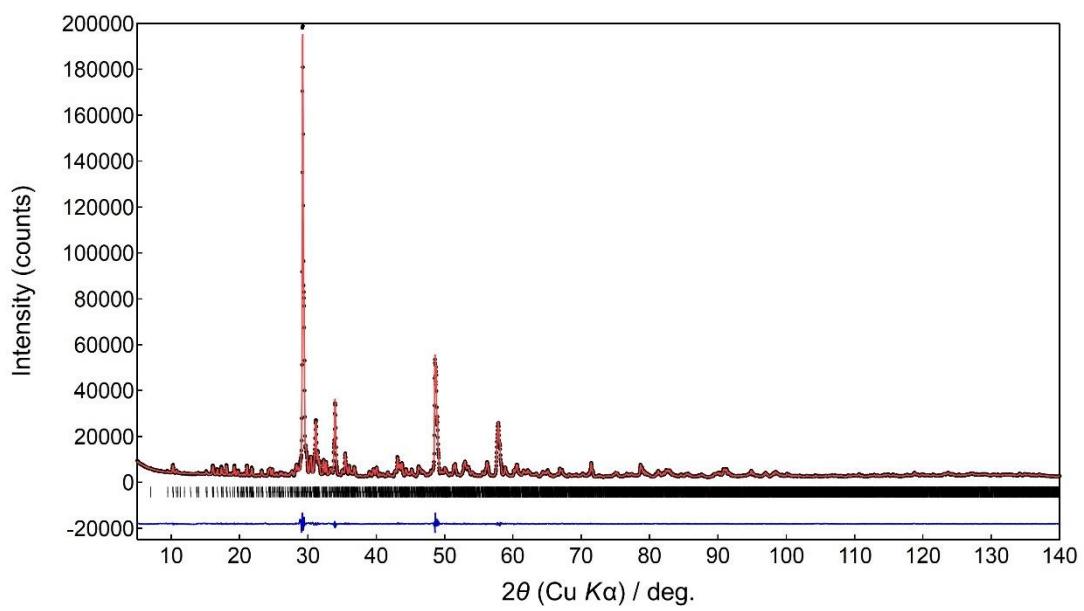


Fig. S4. Experimental (dot) and calculated (solid line) profiles obtained from Rietveld refinement of X-ray powder diffraction data for $\text{BaY}_{16}\text{Si}_4\text{O}_{33}$ at 298 K. The difference profile (bottom) is on the same scale. Vertical ticks indicate the calculated positions of all possible Bragg reflections for $\text{BaY}_{16}\text{Si}_4\text{O}_{33}$.

Table S1 Crystallographic data for BaY₁₆Si₄O₃₃, as derived from Rietveld refinement of powder XRD data.

| | | |
|--|---|---------------|
| Chemical formula | BaY ₁₆ Si ₄ O ₃₃ | |
| Temperature, T (K) | 298(2) | |
| Crystal system | monoclinic | |
| Space group | $P12_1/c1$ (No.14) | |
| Unit-cell dimensions | | |
| | a (Å) | 9.112340(80) |
| | b (Å) | 18.73111(19) |
| | c (Å) | 18.31827(17) |
| | β | 109.04410(66) |
| Unit-cell volume, V (Å ³) | 2955.511(49) | |
| Z | 4 | |
| Calculated density, D_{cal} (Mg m ⁻³) | 4.944526(82) | |
| Radiation wavelength, λ (Å) | 1.54059/1.54432 | |
| 2 θ range for date collection (°) | 5.0 – 140.0 | |
| Reflections collected | 5483 | |
| R_p , R_{wp} | 0.0221, 0.0303 | |
| R_B | 0.00752 | |

$R_p = \sum |Y_{o,m} - Y_{c,m}| / \sum Y_{o,m}$, $R_{wp} = [\sum w_m (Y_{o,m} - Y_{c,m})^2 / \sum w_m Y_{o,m}^2]^{1/2}$, $w_m = 1/\sigma(Y_{o,m})$, $R_B = \sum |I_{o'',k} - I_{c,k}| / \sum I_{o'',k}$, where $Y_{o,m}$ and $Y_{c,m}$ are the observed and calculated data, respectively at data point m ; $\sigma(Y_{o,m})$ is the error in $Y_{o,m}$, and $I_{o'',k}$ and $I_{c,k}$ are the observed and calculated intensities of the k th reflection.

Table S2 Atomic coordinates and overall isotropic displacement parameter (U_{iso}), as derived from Rietveld refinement of powder XRD data for $\text{BaY}_{16}\text{Si}_4\text{O}_{33}$.

| Atom | Wyckoff site | Occ. | x | y | z | U_{iso} |
|------|--------------|------|------------|------------|------------|------------------|
| Ba1 | 4e | 1 | 0.0518(4) | 0.3484(3) | 0.2131(2) | 0.417(17) |
| Y1 | 4e | 1 | 0.0269(7) | 0.1413(4) | 0.0850(3) | 0.417 |
| Y2 | 4e | 1 | 0.0431(8) | 0.5519(4) | 0.1092(4) | 0.417 |
| Y3 | 4e | 1 | 0.0655(8) | 0.5470(4) | 0.5884(4) | 0.417 |
| Y4 | 4e | 1 | 0.0754(7) | 0.7514(4) | 0.1098(4) | 0.417 |
| Y5 | 4e | 1 | 0.2156(7) | 0.0312(3) | 0.2848(4) | 0.417 |
| Y6 | 4e | 1 | 0.2152(6) | 0.6577(4) | 0.3024(3) | 0.417 |
| Y7 | 4e | 1 | 0.2859(7) | 0.3462(5) | 0.4711(3) | 0.417 |
| Y8 | 4e | 1 | 0.3330(6) | 0.1417(3) | 0.4601(3) | 0.417 |
| Y9 | 4e | 1 | 0.3940(8) | 0.4480(4) | 0.1514(4) | 0.417 |
| Y10 | 4e | 1 | 0.3996(9) | 0.2518(4) | 0.1474(5) | 0.417 |
| Y11 | 4e | 1 | 0.4054(8) | 0.0583(4) | 0.1499(4) | 0.417 |
| Y12 | 4e | 1 | 0.5283(6) | 0.3461(5) | 0.3357(3) | 0.417 |
| Y13 | 4e | 1 | 0.5941(7) | 0.1375(4) | 0.3391(4) | 0.417 |
| Y14 | 4e | 1 | 0.6510(9) | 0.0608(4) | 0.0106(4) | 0.417 |
| Y15 | 4e | 1 | 0.6560(9) | 0.2475(4) | 0.0109(4) | 0.417 |
| Y16 | 4e | 1 | 0.6871(8) | 0.4544(4) | 0.0219(4) | 0.417 |
| Si1 | 4e | 1 | 0.0504(19) | 0.3464(14) | 0.0466(10) | 0.417 |
| Si2 | 4e | 1 | 0.200(2) | 0.2139(10) | 0.3000(12) | 0.417 |
| Si3 | 4e | 1 | 0.212(2) | 0.4819(10) | 0.3066(11) | 0.417 |
| Si4 | 4e | 1 | 0.7103(19) | 0.3434(12) | 0.2046(10) | 0.417 |
| O1 | 4e | 1 | 0.028(4) | 0.351(3) | 0.4586(19) | 0.417 |
| O2 | 4e | 1 | 0.031(4) | 0.934(2) | 0.434(2) | 0.417 |
| O3 | 4e | 1 | 0.046(5) | 0.1836(19) | 0.225(2) | 0.417 |
| O4 | 4e | 1 | 0.066(4) | 0.784(2) | 0.458(2) | 0.417 |
| O5 | 4e | 1 | 0.064(5) | 0.504(2) | 0.233(2) | 0.417 |
| O6 | 4e | 1 | 0.056(4) | 0.144(3) | 0.4557(19) | 0.417 |
| O7 | 4e | 1 | 0.095(5) | 0.552(2) | 0.480(2) | 0.417 |
| O8 | 4e | 1 | 0.150(5) | 0.436(2) | 0.366(2) | 0.417 |
| O9 | 4e | 1 | 0.155(4) | 0.043(2) | 0.166(2) | 0.417 |
| O10 | 4e | 1 | 0.168(4) | 0.647(3) | 0.1692(19) | 0.417 |
| O11 | 4e | 1 | 0.164(4) | 0.8317(19) | 0.205(2) | 0.417 |
| O12 | 4e | 1 | 0.158(5) | 0.256(2) | 0.360(2) | 0.417 |
| O13 | 4e | 1 | 0.218(5) | 0.048(2) | 0.403(2) | 0.417 |
| O14 | 4e | 1 | 0.217(4) | 0.357(3) | 0.0937(18) | 0.417 |
| O15 | 4e | 1 | 0.266(5) | 0.536(2) | 0.099(3) | 0.417 |

| | | | | | | |
|-----|------|---|----------|------------|------------|-------|
| O16 | $4e$ | 1 | 0.259(4) | 0.155(3) | 0.0943(19) | 0.417 |
| O17 | $4e$ | 1 | 0.333(4) | 0.433(2) | 0.262(2) | 0.417 |
| O18 | $4e$ | 1 | 0.301(4) | 0.140(2) | 0.3368(19) | 0.417 |
| O19 | $4e$ | 1 | 0.310(5) | 0.269(2) | 0.258(2) | 0.417 |
| O20 | $4e$ | 1 | 0.420(5) | 0.062(2) | 0.036(2) | 0.417 |
| O21 | $4e$ | 1 | 0.411(5) | 0.2612(18) | 0.033(3) | 0.417 |
| O22 | $4e$ | 1 | 0.442(5) | 0.4548(19) | 0.036(2) | 0.417 |
| O23 | $4e$ | 1 | 0.446(5) | 0.032(2) | 0.287(2) | 0.417 |
| O24 | $4e$ | 1 | 0.499(4) | 0.342(2) | 0.4392(18) | 0.417 |
| O25 | $4e$ | 1 | 0.540(4) | 0.345(3) | 0.2046(19) | 0.417 |
| O26 | $4e$ | 1 | 0.538(4) | 0.163(2) | 0.224(2) | 0.417 |
| O27 | $4e$ | 1 | 0.565(4) | 0.142(2) | 0.4530(19) | 0.417 |
| O28 | $4e$ | 1 | 0.660(5) | 0.443(2) | 0.387(2) | 0.417 |
| O29 | $4e$ | 1 | 0.690(5) | 0.250(2) | 0.394(3) | 0.417 |
| O30 | $4e$ | 1 | 0.664(5) | 0.041(2) | 0.147(2) | 0.417 |
| O31 | $4e$ | 1 | 0.700(5) | 0.270(2) | 0.152(2) | 0.417 |
| O32 | $4e$ | 1 | 0.748(4) | 0.411(2) | 0.162(2) | 0.417 |
| O33 | $4e$ | 1 | 0.791(4) | 0.164(2) | 0.098(2) | 0.417 |