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Supporting information for article:

Texture-based residual stress analysis of laser powder bed fused Inconel 718 parts

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Technique	radiation	reflection Diffraction angle	ψ/χ-tilting (steps)	φ-tilting (steps)	assumptions
Laboratory XRD Xstress G3	Monochromatic, Mnkα	Ni-311 20 ≈ 156°	-45° to 45° (19)	0°, 90°	Top: $\sigma_{i3} = 0$ $\sigma_{12} = 0$ Side: $\sigma_{i1} = 0$ $\sigma_{23} = 0$
Synchrotron XRD P61A	Energy dispersive, 30 - 200 keV	Ni - 311 E ≈ 55 keV 20 ≈ 11.946°	0 to 80° (20)	0 - 360° 3, 7, 8 ,9 (5°) 1, 2, 4, 5 (15°)	-
Neutron diffraction POLDI Neutron diffraction KOWARI	Time of flight, $Q \approx 1-8 \ 2\pi d^{-1}$ Monochromatic, $\lambda = 1.53 \ \text{\AA}$	$2\theta \approx 90^{\circ} \pm$ 15° Ni-311 $2\theta \approx 90^{\circ}$	2 orthogonal directions (BD, T) 3 orthogonal directions (BD, T, L)		-

 Table S1: Overview of the measurement conditions for the different diffraction techniques.

Table S2: Obtained eigenvalues for the top surfaces of the specimen $H_{0^{\circ}}$ and $H_{45^{\circ}}$ according to the measurement positions 1-9 acquired by energy dispersive synchrotron diffraction.



H _{45°}	#d ³¹¹	σ' _T -σ' _{BD} /MPa	σ'l-σ'bd /MPa	φ _p /°	H _{0°}	#d ³¹¹	σ' _T -σ' _{BD} /MPa	σ'l-σ'bd /MPa	φ _p /°
1	381	414 ± 18	265 ± 18	21.9 ± 3.6	1	384	392 ± 20	300 ± 20	8.3 ± 7
2	382	381 ± 18	46 ± 17	8.8 ± 1.1	2	384	393 ± 19	172 ± 19	-1.0 ± 0.8
3	1863	255 ± 8	57 ± 8	18.5 ± 1.1	3	1833	384 ± 9	178 ± 9	0 ± 0.6
4	382	367 ± 17	92 ± 17	12.3 ± 1.4	4	384	383 ± 18	154 ± 17	4.2 ± 1.4
5	377	387 ± 19	209 ± 19	17.6 ± 2.8	5	383	371 ± 18	256 ± 17	7.5 ± 3.3
H _{45°}	#d ³¹¹	σ' _{BD} -σ' _T /MPa	σ' _L -σ' _T /MPa	φ _p /°	H _{0°}	#d ³¹¹	σ' _{BD} -σ' _T /MPa	σ' _L -σ' _T /MPa	φ _p /°
7	1511	265 ± 9	12 ± 7	-0.5 ± 0.7	7	1512	391 ± 10	96 ± 9	-1.3 ± 0.5
8	1512	257 ± 9	17 ± 7	$\textbf{-2.4}\pm0.6$	8	-	-	-	-
9	1512	278 ± 8	10 ± 4	$\textbf{-2.0}\pm0.6$	9	1512	399 ± 10	61 ± 8	$\textbf{-4.2}\pm0.5$